

# A 360mm f/19 Kutter Schiefspiegler

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HOME



# AUSTRALIA







Population 4.9 million





18 Myddleton Drive  
Heidelberg

$145.1^{\circ}$  East  
 $37.8^{\circ}$  south



# Sky and TELESCOPE

## *In This Issue:*

Moon Photographs  
with an Off-Axis  
Reflector

Eclipse Observations  
on October 12th

Jai Singh and His  
Observatory  
at New Delhi

Some Possible Evidence  
of Evolution  
in Individual Stars

Solar Research Reported  
at Moscow

The Cateye

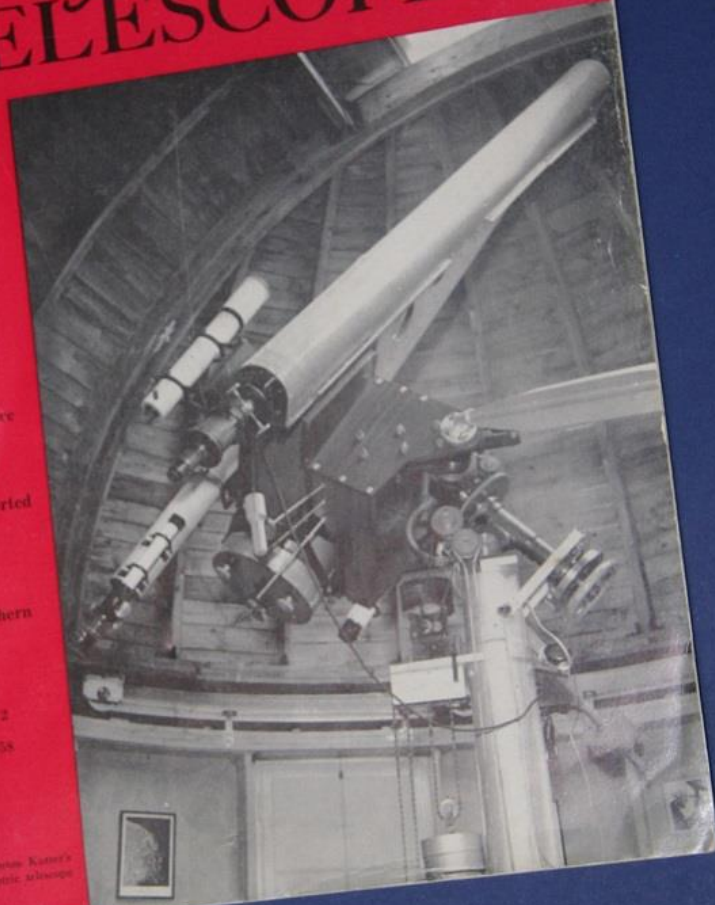
Northern and Southern  
Star Charts

★  
Vol. XVIII, No. 2

DECEMBER, 1958

50 cents

★  
Astoria, Oregon  
Published by Sky and Telescope, Inc.





grinding the wetted primary was checked by the Foucault test. It is important to hold the radius of curvature to 1-inch tolerance if the indicated dimensions are to be used. Remember, too, that it is more difficult to achieve a good long-focus sphere than one of average focal length.

Polishing was done in the usual manner, except that another plate glass disk was used for backing the pitch lap. Because of the very shallow curve required, this disk may be left flat if a good  $\frac{1}{4}$  inch of pitch is poured on it. And after the primary was completed, the secondary, still  $4\frac{1}{2}$  inches in diameter, was hot-pressed onto the same pitch lap, which quickly conformed to the shallow reverse curve.

During polishing, the convex surface was periodically tested through its flat back, using two thirds of the radius of curvature for the knife-edge position. . . . The surface could also have been checked by interference fringes if it were fitted against the concave primary.

The final biscuit cut was made through the secondary's finished surface, which was protected from grit by two layers of masking tape. Care was needed to assure alignment of this cut with the one coming from the back. But the secondary did not suffer from the carborundum used in cutting, nor did it have a turned-down edge. It would have been difficult to achieve this result if the mirror had been ground after cutting it to size.

For the mounting, a full-sized layout should be scaled up from the drawing. The mahogany cradle (see Fig. 84) was made at a mill; I bored out the 3-inch hole in the lathe and made the  $\frac{1}{4}$ -inch saw cut later. The  $\frac{1}{4}$ -inch side pieces were left somewhat larger and were cut only after checking with the full-sized layout. A large piece of sandpaper was stretched over the curve of the primary tube, and the side pieces were lapped to it after being screwed to the cradle. Six little wood screws inside the tube secure it to the side pieces. The distance  $\Delta'$  between the center of the primary mirror and the optical axis of the secondary's reflection must be precisely 8 inches. This is built into the mount, so it is very important to preserve it by fitting the side pieces and the tube together carefully.

After it is tilted into position, the secondary must be concentric with the 3-inch tube. I accomplished this by drilling the central hole in the back of the turned aluminum cell  $\frac{1}{4}$ -inch below center. The  $\frac{1}{2}$ -inch bolt that fits this hole is swivel-mounted in the cell to afford the play necessary for tilt adjustment. A compression spring holds the cell firmly against three pointed adjusting screws that fit into small cup-shaped recesses in the back of the cell. These screws are threaded into tapped holes in the backing plates. In both primary and secondary cells, one



FIG. 84. Oscar Knab's mahogany and jeweled-aluminum Schiefspiegler (oblique reflector) on its altazimuth mounting is particularly valuable for lunar and planetary observing because of its excellent image quality. It is less well suited for viewing dim extended objects, such as galaxies and nebulae, because its focal ratio is high.

of the adjusting screws must be in the mounting's meridional plane, as indicated by the *M* in the end view of the secondary cell (Fig. 83).

The curved cutout in the secondary tube was done with a wire-bladed hacksaw and then filed smooth. The slanted cutoff at the mirror end of this tube was made with the end plate of the cell fastened in place, facilitating cutting by stiffening the end. The tubes were blackened inside with two coats of blackboard slating and were machine-jeweled on the outside with steel wool wrapped around a rubber-capped wooden dowel in a drill press, and then lacquered. The mahogany received several coats of clear spar varnish.

For rough adjustment, place a tube with a  $\frac{1}{4}$ -inch eye hole into the eyepiece holder, and tilt the secondary by means of the three adjusting screws until the primary cell shows concentrically in the secondary mirror. This need never be repeated. To set the primary, tape a  $4\frac{1}{2}$ -inch cardboard disk just under the secondary tube at its outer end, to indicate the direction of the rays that will enter the primary. Direct the primary until it looks squarely at this disk, and rough adjusting is completed.

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There are three devices to change the above mentioned fundamental system into a Schiefspiegler:  
 1) the anastigmatic, 2) the coma-free, 3) the ostadloptical device.

1) The anastigmatic device (former called 'The Neo-Brachy')  
 (All symbols vide fig.2)

The inclination  $\varphi_1$  of the incoming parallel beam of rays is determined by the condition for freedom of silhouetting. It must be the 'first ax-distance'

$$1) \Delta = y_1 + y_2$$

$$2) \sin 2\varphi_1 = \frac{\Delta}{e}$$

If this excentrical system is to be free from astigmatism the inclination  $\varphi_2$  of the secondary must become

$$3) \sin \varphi_2 = \sin \varphi_1 \cdot \frac{y_1}{y_2} \sqrt{\frac{r_1}{r_2}}$$

When  $r_1$  equals  $r_2$  the formula 3) is simplified to

$$3a) \sin \varphi_2 = \sin \varphi_1 \cdot \frac{y_1}{y_2}$$

with  $\varphi_2$  the 'second ax-distance'  $\Delta'$  (important for the construction of the Schiefspiegler) is determined

$$4) \Delta' = e \cdot \sin 2\varphi_2$$

The inclination  $\varphi_2$  of the secondary eliminates the astigmatism of the oblique beam of rays coming from the primary, but isn't sufficient to abolish thoroughly its coma too. It remains therefore a residual coma

$$5) \beta = 3 \cdot y_2^2 \left[ \sin \varphi_1 \cdot \left( \frac{1}{r_1} \right)^2 + \left( \frac{y_1}{y_2} \right)^2 \cdot \sin \varphi_2 \cdot \left( \frac{1}{r_1} + \frac{1}{r_2} \right) \cdot \frac{1}{r_2} \right]$$

Note: Calculation with the slide rule will do.  $r_2$  is to be introduced with negative sign. The value of  $\beta$  results in the arcus of the angle. To get the angle  $\beta$  in seconds of arc multiply the result with the factor 206265. The accuracy of the result is very high and reaches that of a logarithmic-trigonometrical computation (7 places) within  $\pm 1 - 2\%$ . (Note  $206265 = 180^\circ \times 60 \times 60$ , arcus = radian)

For the above mentioned fundamental system the residual coma results of about  $+4\%$  (undercorrected). This value changes only slowly in moderate changing the dimensions A, b of our fundamental system, but diminishes and enlarges rapidly by diminishing or enlarging the aperture ratio of the primary.

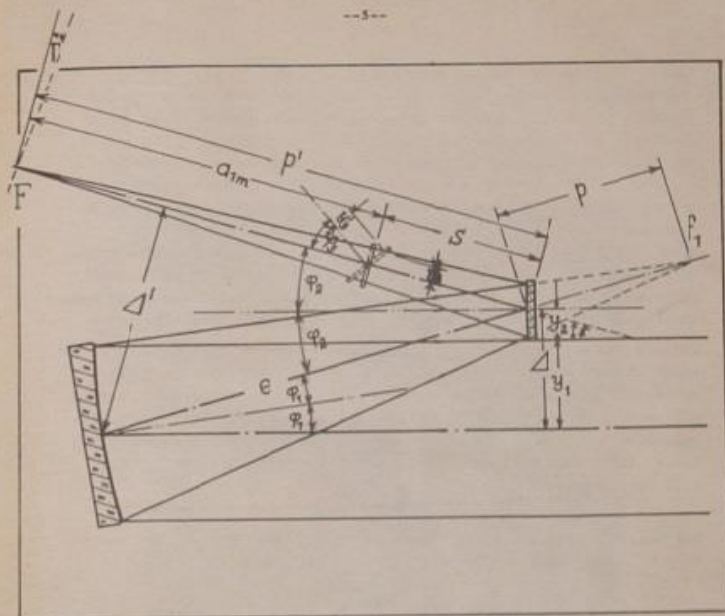


Fig.2 SCHEME OF THE SCHIEFSPIEGLER

Symbols

- $\varphi_1$  inclination of the primary
- $\varphi_2$  inclination of the secondary
- $\varphi_3$  inclination of the corrector lens
- $\Delta$  the first axis-distance
- $\Delta'$  the second axis-distance
- $y_3$  radius of the cone of light on the corrector-lens
- $y_2$  radius of the corrector-lens
- $s_{1m}$  distance of the corrector lens from the meridional focus
- $s$  distance of the corrector lens from the secondary
- $\delta$  variation-angle
- $\Gamma$  angle of the extended field of view toward the eyepiece's focal-plane.

All other symbols v. fig.1



105mm f/25  
Anastigmatic Schiefspiegler  
1968















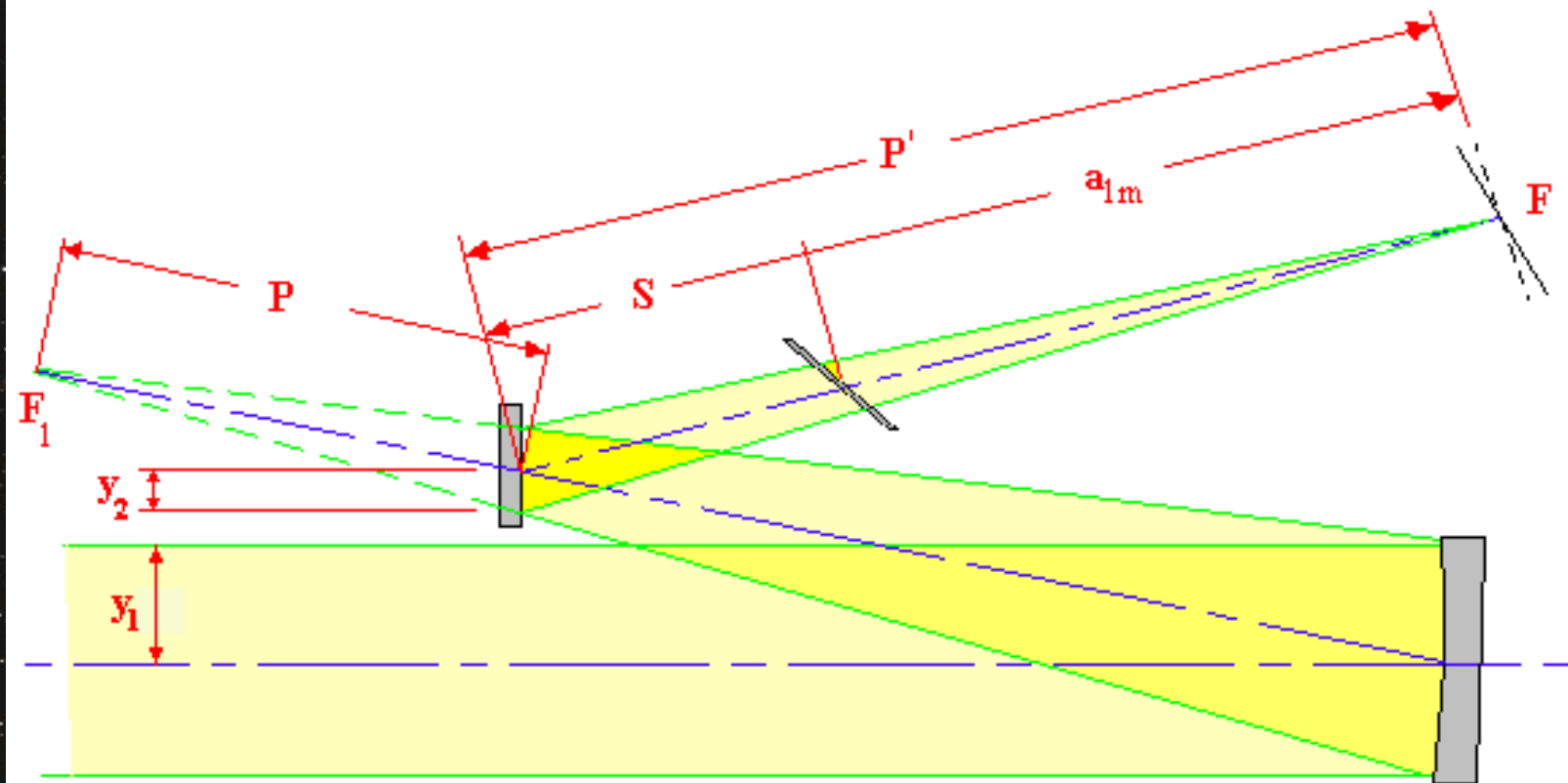






# 315mm Kutter Schiefspiegler 1969

## Schiefspiegler definition of terms





# The Observatory



3.35 metre (11 feet) diameter  
Fibre glass dome.

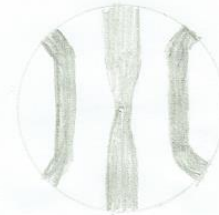


5 minutes.

3" Strokes with ~~or~~ 2 lap  
of pressure over edge  
(lie on edge of mirror)



Changed to Rouge  
Same as above.

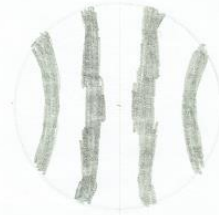


Same as above.



4 Minutes.

Long strokes. (3"  
pressure over edge for 2 laps.  
Surface is getting uneven.  
Polish with parabolizing  
strokes for 3 laps X



10 minutes  
3" stroke.  
cerium oxide.  
No change





# Secondary Cell

Fibre glass





# Lens Cell



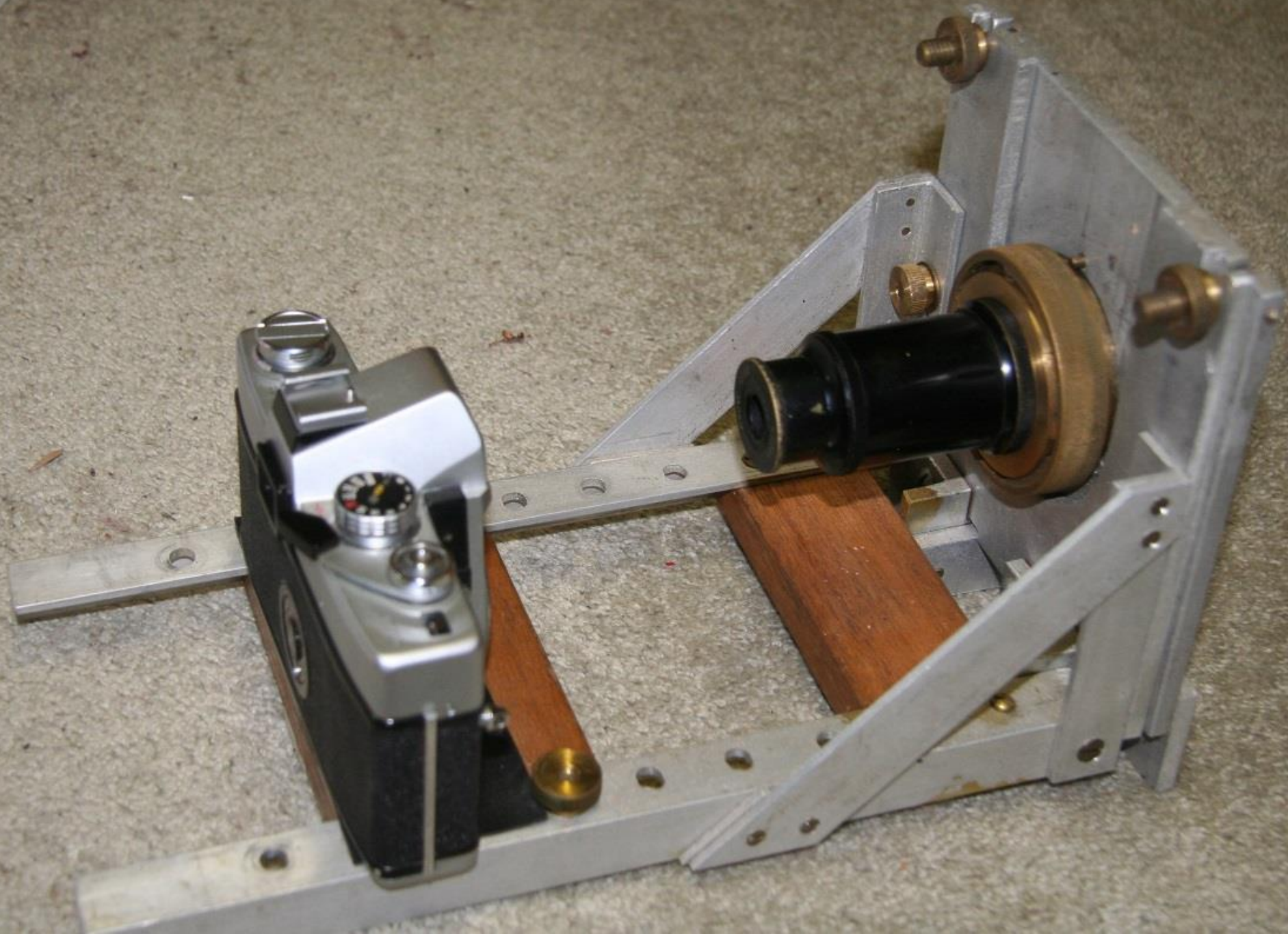














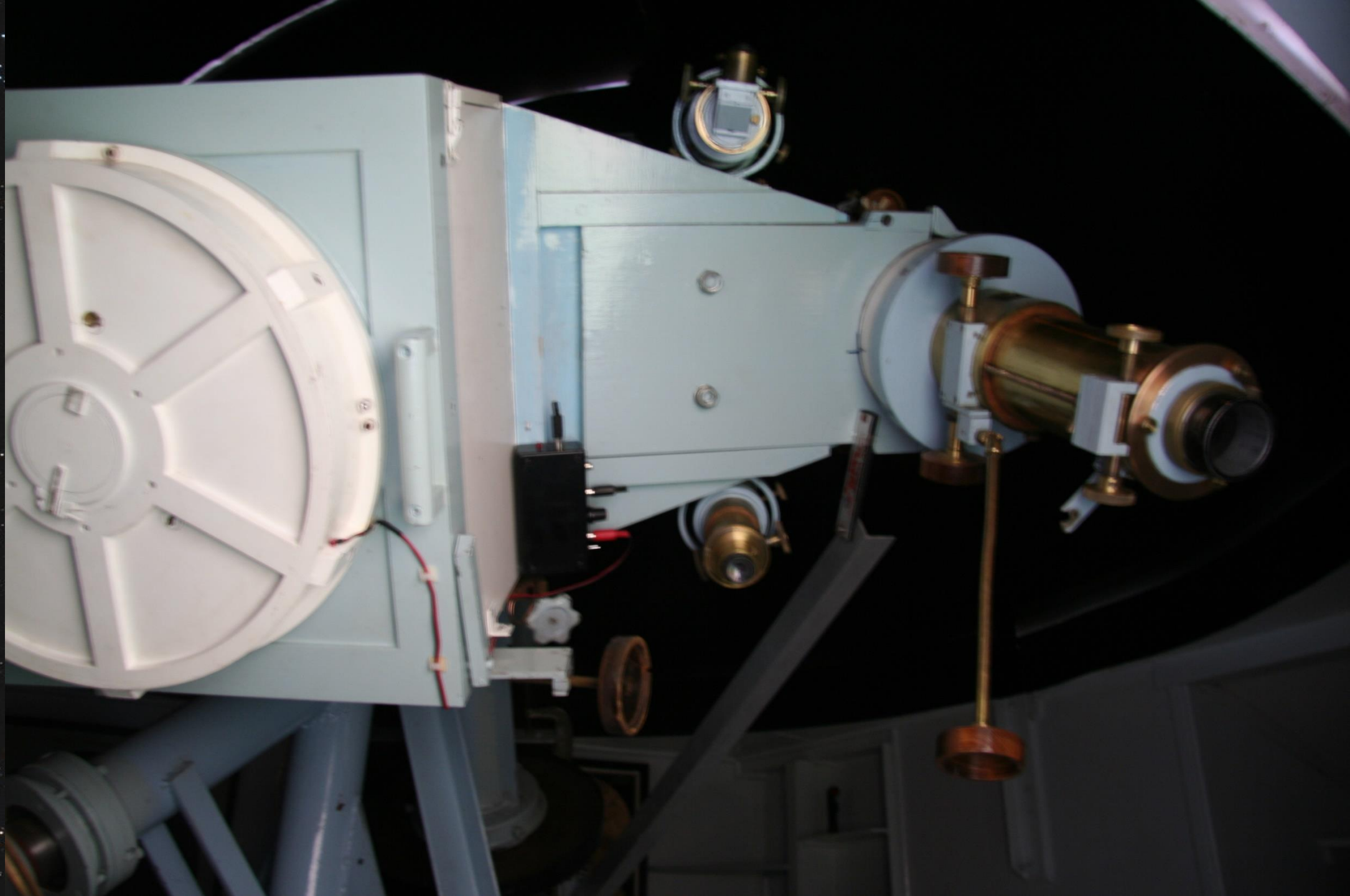
# The drive













**Primary**

**Material :- BVC**

$R_1 = 8200$  mm. Diameter  
 $D_1 = 360$  mm.

Thickness (edge) =

$F_1 = 4100$  mm.  
f/ratio = f/11.389

**Secondary**

**Material:- Zerodur**

**(see notes under optical work)**

$R_2 = 8300$  mm.  
Diameter  $D_2 = 155.28$  mm.

Thickness (edge) =

**Tertiary** (tilted lens)  
512605

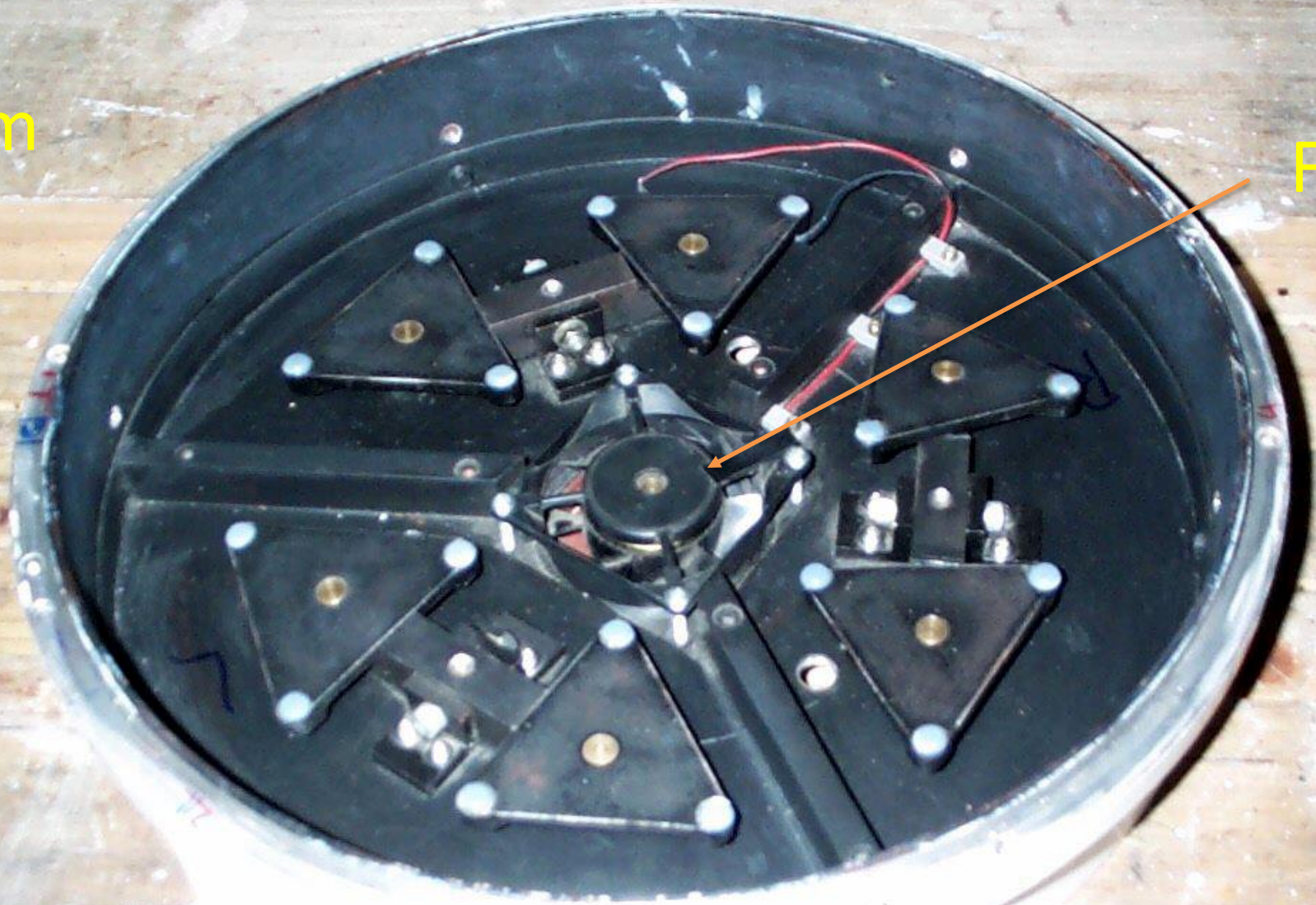
**Material:- C2**

$F_3 = 73000$  mm.  
Diameter  $D_3 = 130.08$  mm.



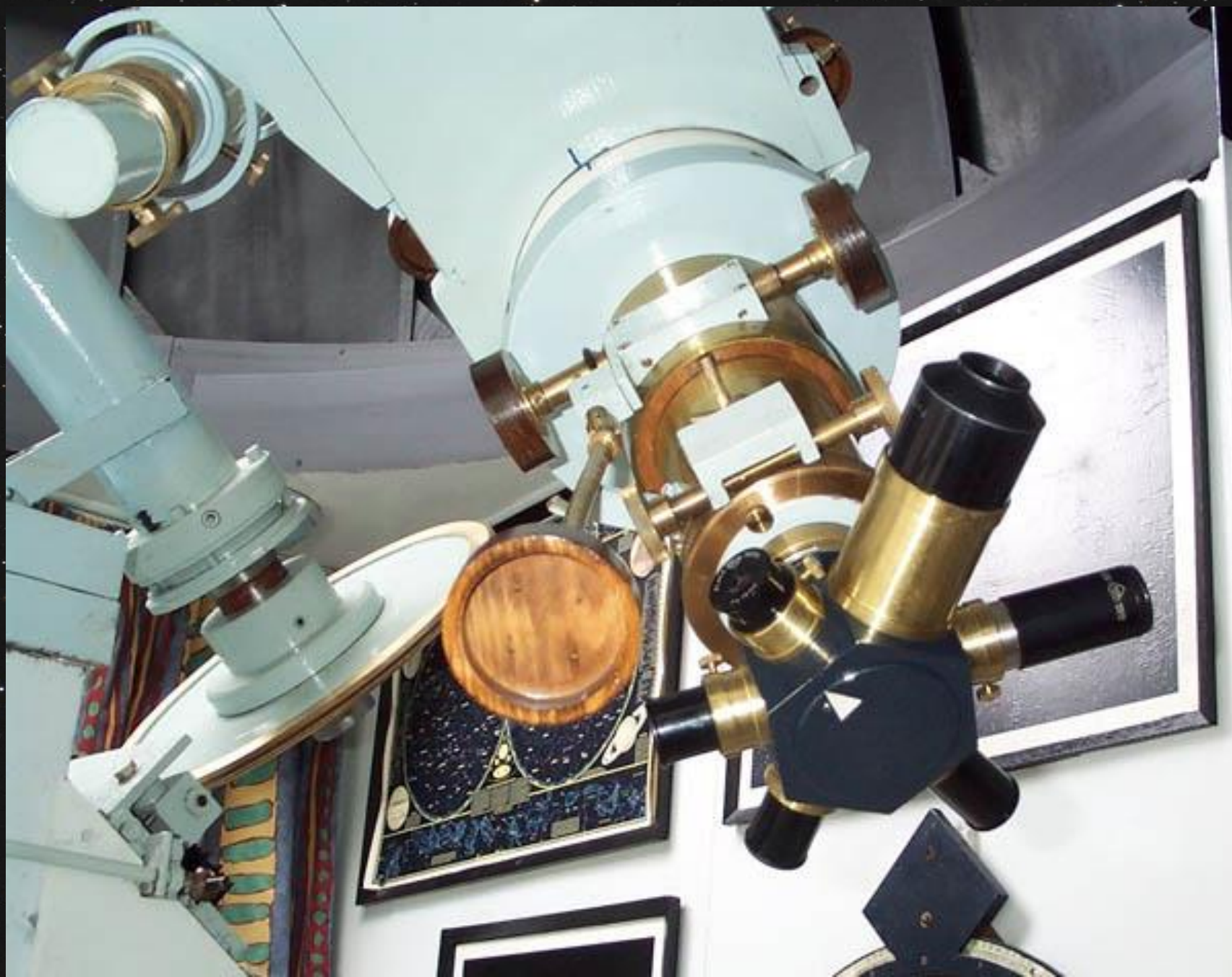
Aluminium

Fan

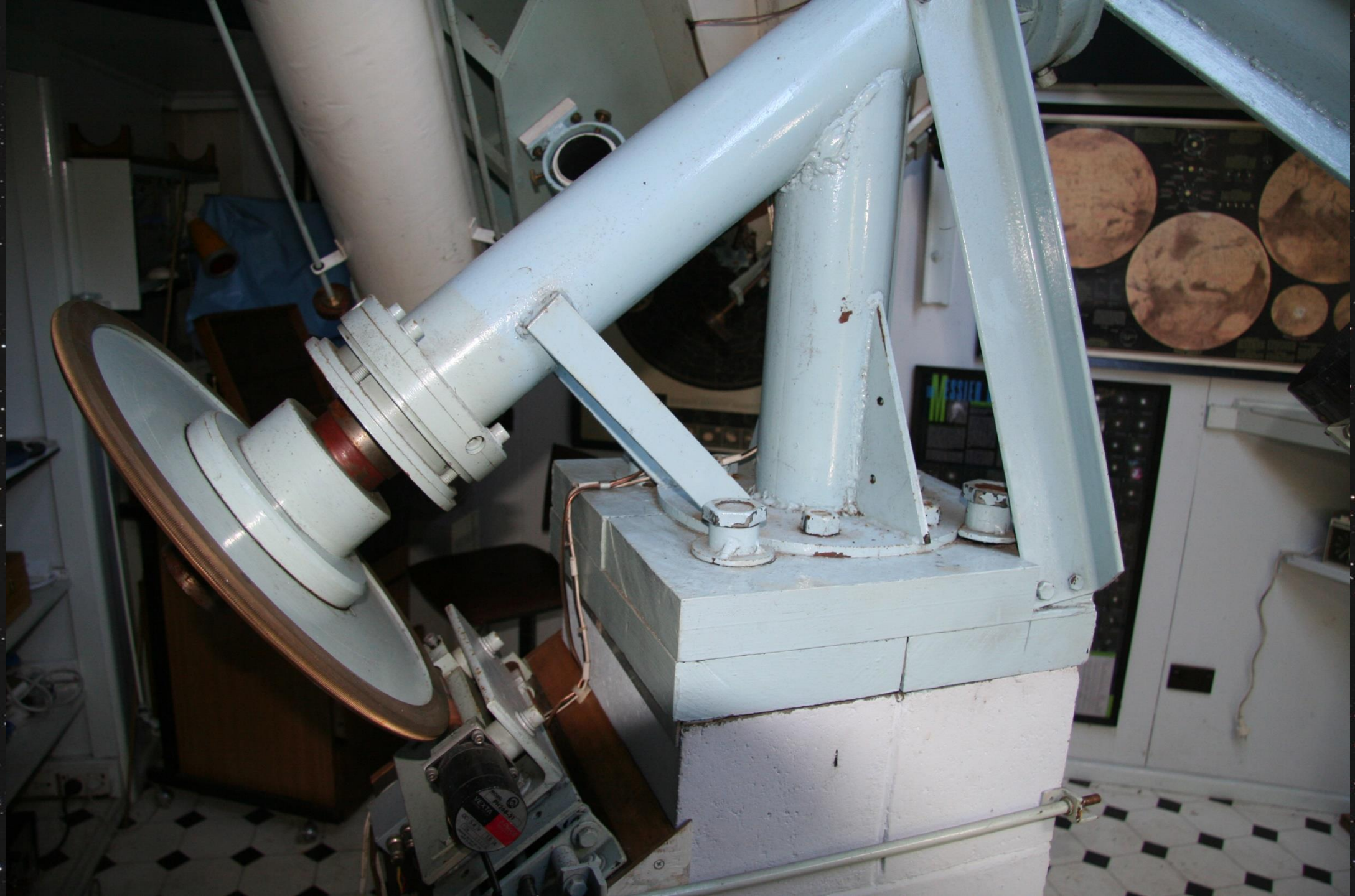


30. 6. 2003



















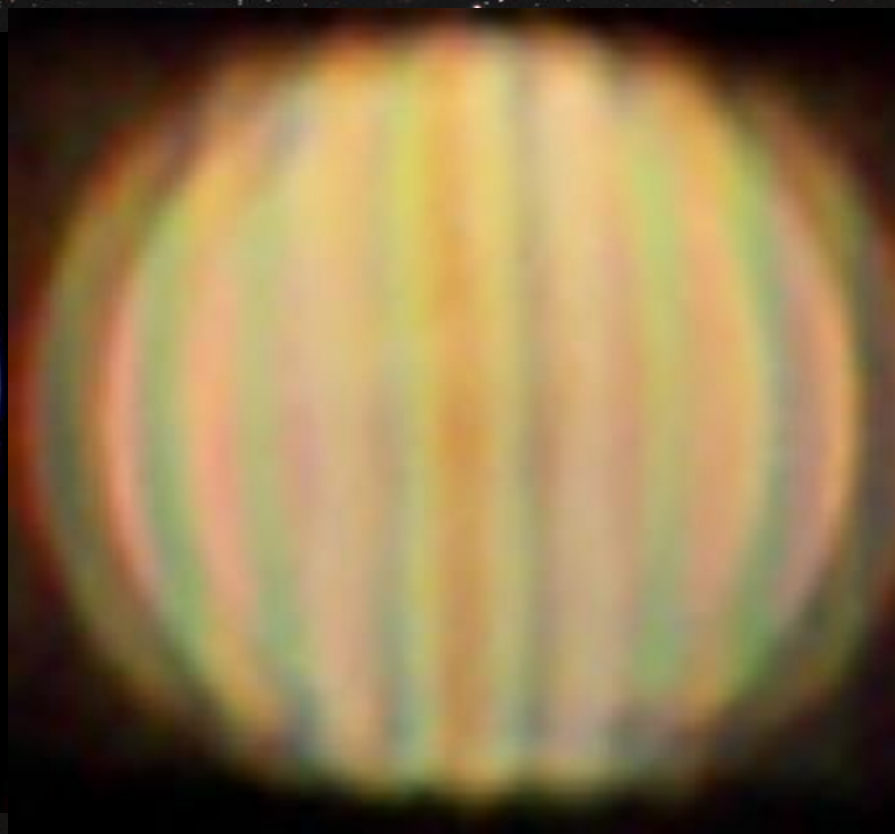
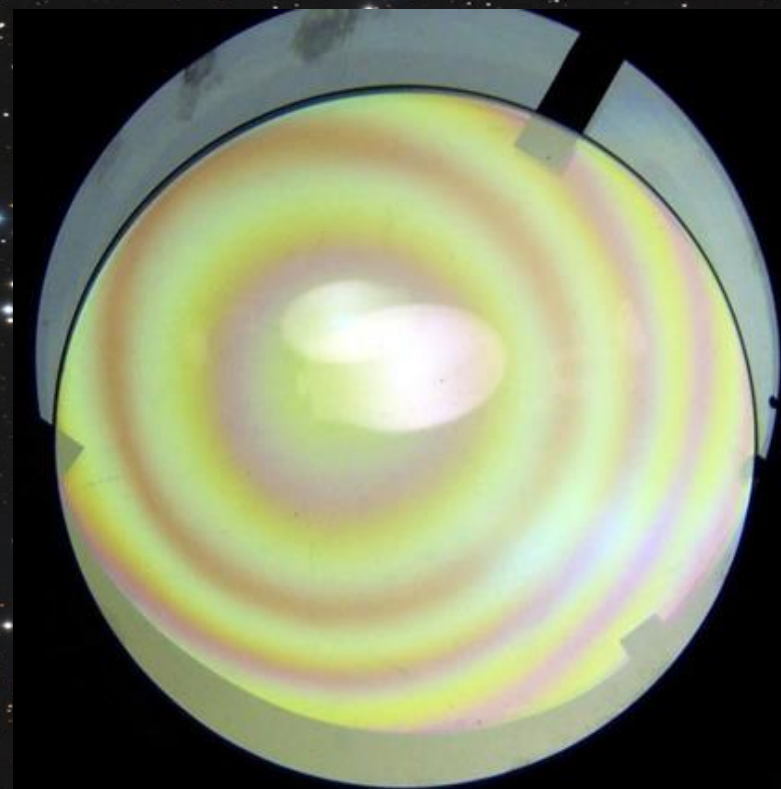
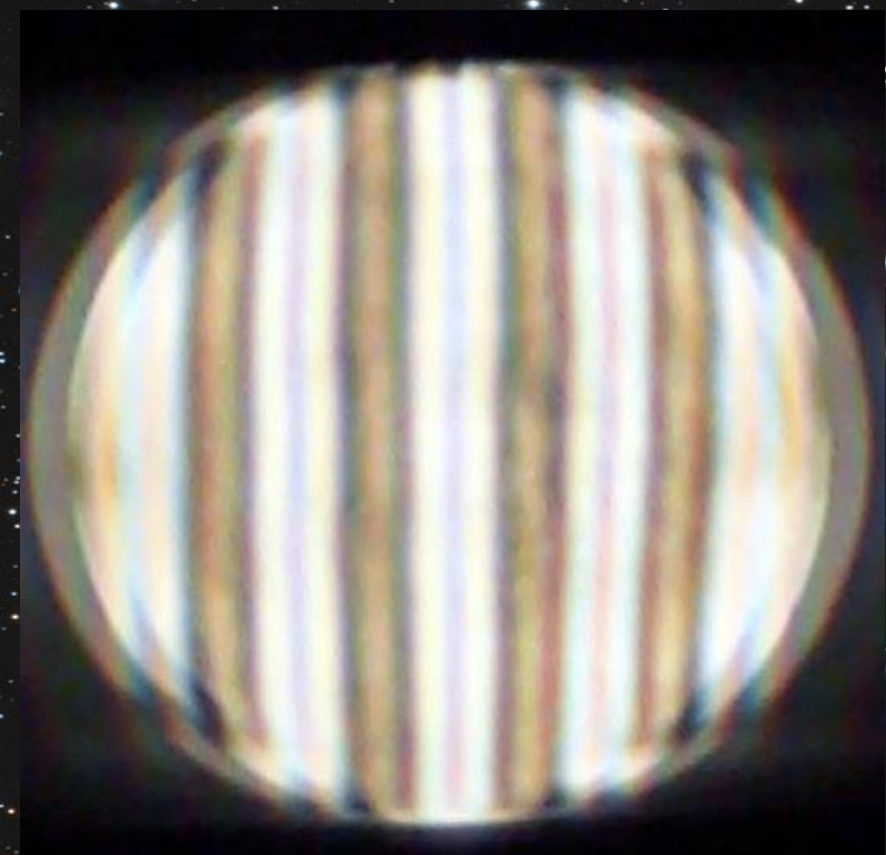


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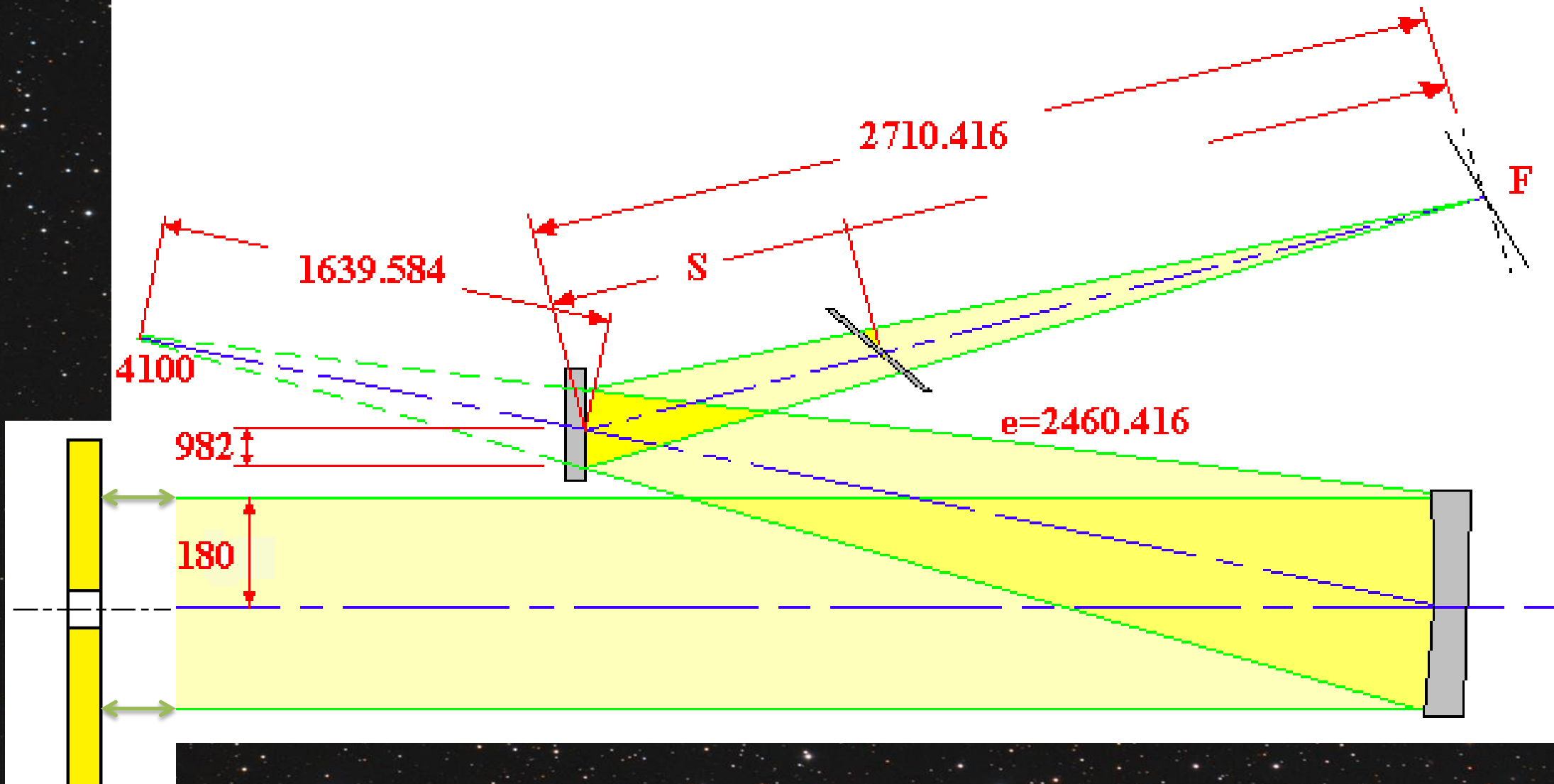








# Summary









approximate internal radius  
of observatory = 1.6 m.

6mm  
clearance  
to back of  
adjusting screws

tube 2200

160

125

220  
183

320  
190

600  
100

340  
97

13°

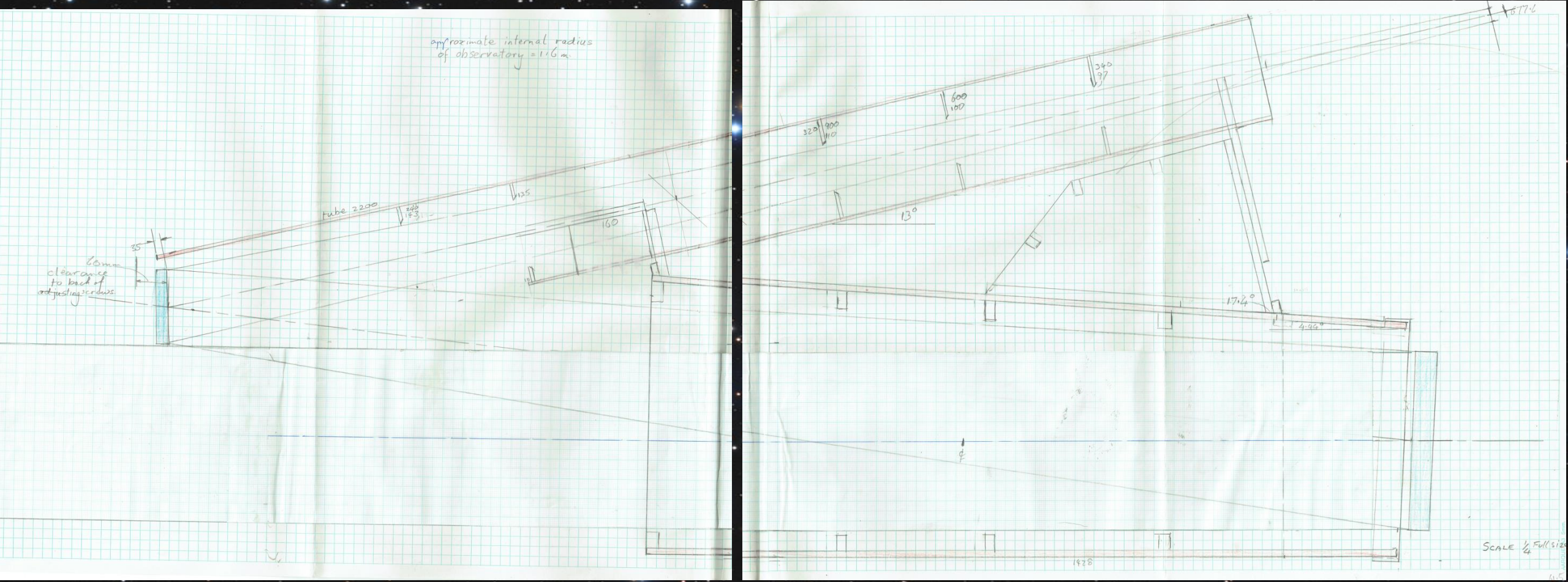
17.4°

4.45°

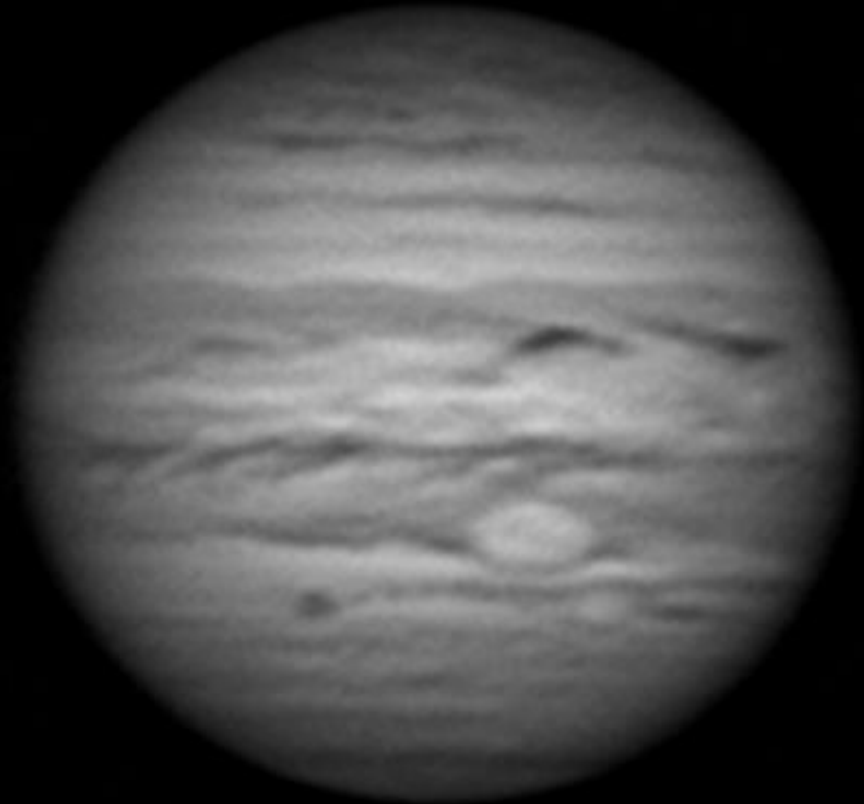
Scale 1/4 Full size

1428

577.6







2008-07-23\_09-47-25







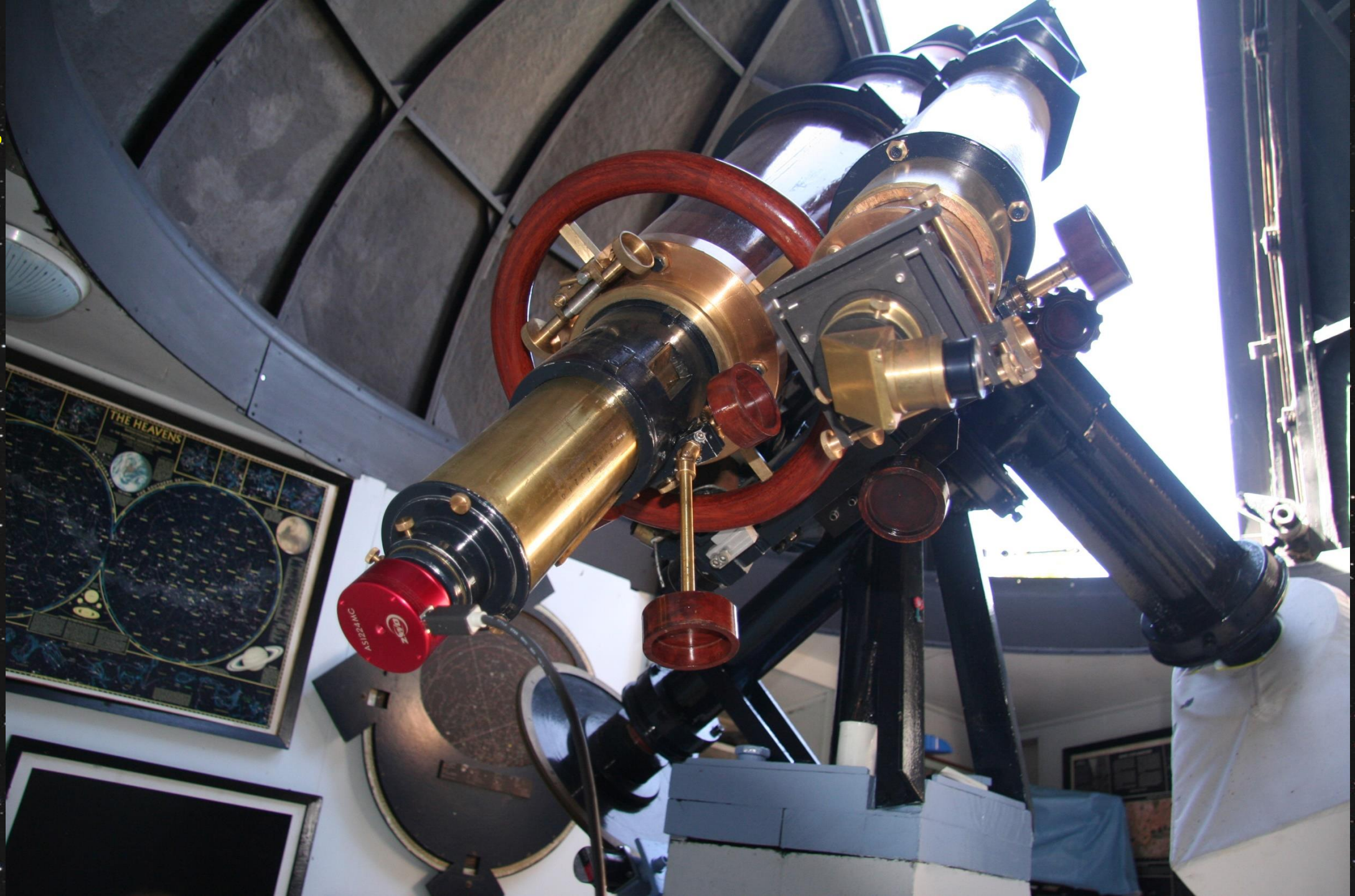








2







RGB  
17-34-20



17-44-23  
600x40nm



17-47-46  
800x40nm



17-50-45  
600x40nm

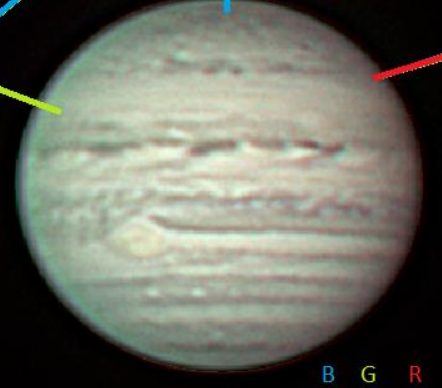


17-53-53  
700x40nm

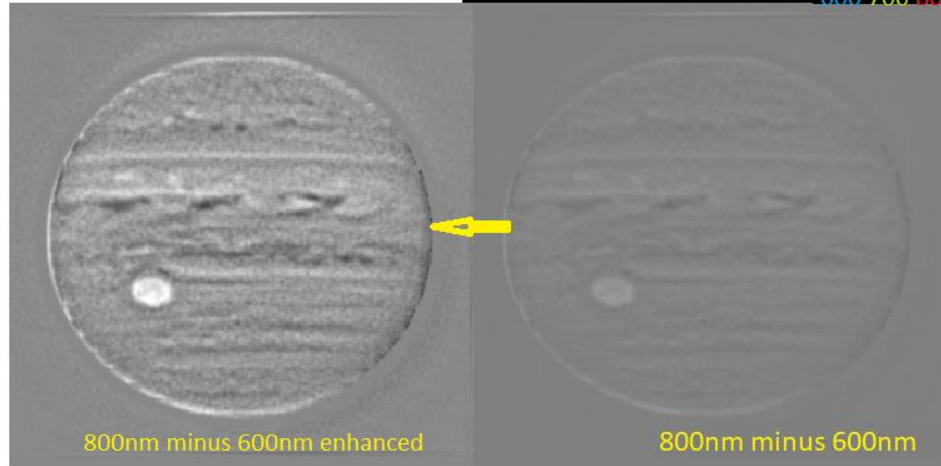
6 March 2018



B G R  
600 700 800



B G R  
700 800 950



800nm minus 600nm enhanced

800nm minus 600nm



A dark, starry night sky with numerous stars of varying colors (white, blue, orange) and sizes. The text "Questions ??" is centered in a bright yellow font.

Questions ??